

JC19 Rec'd PCT/PTO 24 MAY 2001

FORM PTO-1390 DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE
(REV 11-2000)

**TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371**

ATTORNEY'S DOCKET NO

970054.406USPC

U.S. APPLICATION NO. (If known, see 37 CFR 1.5)

Unknown

09/856654

INTERNATIONAL APPLICATION NO.

PCT/EP99/07655

INTERNATIONAL FILING DATE

12 October 1999 (12.10.1999)

PRIORITY DATE CLAIMED

26 November 1998 (26.11.1998)

TITLE OF INVENTION

AZIMUTHAL DRIVING SYSTEM FOR WIND TURBINES

APPLICANT(S) FOR DO/EO/US

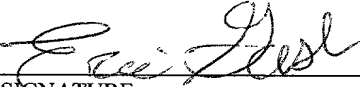
WOBBEN, Aloys

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (21) indicated below.
4. ☒ The US has been elected by the expiration of 19 months from the priority date (Article 31).
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2)).
 - a. ☐ is attached hereto (required only if not communicated by the International Bureau).
 - b. ☒ has been communicated by the International Bureau.
 - c. ☐ is not required, as the application was filed in the United States Receiving Office (RO/US).
6. ☐ An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)).
 - a. ☒ is attached hereto
 - b. ☐ has been previously submitted under 35 U.S.C. 154(d)(4).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)).
 - a. ☐ are attached hereto (required only if not communicated by the International Bureau).
 - b. ☐ have been communicated by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☒ have not been made and will not be made.
8. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. ☒ A English language translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11 to 20 below concern document(s) or information included:

11. ☒ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☐ A **FIRST** preliminary amendment.
14. ☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
15. ☐ A substitute specification.
16. ☐ A change of power of attorney and/or address letter.
17. ☐ A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 – 1.825.
18. ☐ A second copy of the published international application under 35 U.S.C. 154(d)(4)
19. ☒ A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4).
20. ☐ Other items of information:

U.S. APPLICATION NO. (If known, see 37 CFR 1.5)		INTERNATIONAL APPLICATION NO.		ATTORNEY'S DOCKET NUMBER	
Unknown		PCT/EP99/07655		970054.406USPC	
21. <input checked="" type="checkbox"/> The following fees are submitted:				CALCULATIONS	
Basic National Fee (37 CFR 1.492(a)(1)-(5)):				PTO USE ONLY	
Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO \$1000.00					
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO \$860.00					
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO \$710.00					
International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4)..... \$690.00					
International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) \$100.00					
ENTER APPROPRIATE BASIC FEE AMOUNT =				\$860.00	
Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input checked="" type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)).				\$130.00	
Claims	Number Filed	Number Extra	Rate		
Total Claims	6 - 20 =	0	x \$ 18.00	\$0.00	
Independent Claims	1 - 3 =	0	x \$ 80.00	\$0.00	
Multiple dependent claim(s) (if applicable)			+ \$270.00	\$270.00	
TOTAL OF ABOVE CALCULATIONS =				\$1260.00	
<input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2.				\$0.00	
SUBTOTAL =				\$1260.00	
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				\$0.00	
TOTAL NATIONAL FEE =				\$1260.00	
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property				\$0.00	
TOTAL FEES ENCLOSED =				\$1260.00	
				Amount to be refunded:	
				charged	
a. <input checked="" type="checkbox"/> A check in the amount of \$1260.00 cover the above fees is enclosed.					
b. <input type="checkbox"/> Please charge my Deposit Account No. in the amount of \$_ to cover the above fees. A duplicate copy of this sheet is enclosed.					
c. <input checked="" type="checkbox"/> The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 19-1090. A duplicate copy of this sheet is enclosed.					
d. <input type="checkbox"/> Fees are to be charged to a credit card. WARNING: Information on this form may become public. Credit card information should not be included on this form. Provide credit card information and authorization on PTO-2038.					
NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.					
SEND ALL CORRESPONDENCE TO:					
GASH, Eric, J. Seed Intellectual Property Law Group PLLC 701 5 th Avenue, Suite 6300 Seattle, WA 98104-7092 United States of America (206) 622-4900					
 SIGNATURE					
Eric J. Gash NAME					
46,274 REGISTRATION NUMBER					

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JC18 Rec'd PCT/PTO 2 4 MAY 2001

Aloys Wobben, Argestrasse 19, 26607 Aurich

Azimuthal drive for wind power installations

Wind power installations generally have an active drive for wind direction tracking. The active drive rotates the machine housing of the wind power installation in such a way that the rotor blades of the rotor are oriented in the direction of the wind. That drive which is required for wind direction tracking purposes is generally an azimuthal drive which is usually disposed with the associated azimuthal mountings between the tower top and the machine housing. One displacement drive is sufficient when small wind power installations are involved, while larger wind power installations are generally equipped with a plurality of azimuthal drives.

In the procedure involving wind direction tracking of the machine housing, an operating wind-measuring system supplies a mean value for the wind direction over a certain period of time, for example 10 seconds. That mean value is repeatedly compared to the instantaneous azimuthal position of the machine housing. As soon as a deviation exceeds a given value, the machine housing is suitably re-adjusted so that the deviation of the rotor from the wind direction, being the yaw angle, is as small as

possible in order to avoid power losses. The way in which wind direction tracking is implemented in the case of known wind power installations is described in "Windkraftanlagen" ("Wind Power Installations"), Erich Hau, second edition, 1995, pages 268 ff and 316 ff respectively.

In previously known wind power installations, motor-powered wind direction tracking of the machine housing, the azimuthal displacement system, takes over the function of automatically orienting the rotor and the machine housing according to the direction of the wind. When considered functionally, the wind direction tracking system is an independent unit. When considered from the point of view of structure, it forms the transition of the machine housing to the tower top. The components thereof are integrated in part in the machine housing and in part in the tower top. The overall system for wind direction tracking comprises the components consisting of the setting drive, holding brakes, locking device, azimuthal mountings and regulating system. Those components operate as follows:

For the setting drive, there are the alternatives hydraulic or electrical, in a similar manner as for the rotor blade displacement drive. Both design configurations are usual in relation to wind power installations. Small installations mostly have unregulated electrical drive motors. In the case of large installations, hydraulic setting drives are in the majority.

A rotary movement-check arrangement or a yaw brake is required in order to prevent the yaw moment about the axis of rotation having to be maintained after the tracking operation has been effected, by drive motors. Otherwise, the service life of the drive assemblies or the upstream-connected transmission assemblies could scarcely be guaranteed. Small installations are generally satisfied with a rotary movement-check arrangement in the azimuthal mounting, while a plurality of releasable holding brakes are known for larger installations. The holding brakes engage a braking ring at the inside of the tower or

conversely a ring on the machine housing. During the tracking operation one or two azimuthal brakes are in engagement in order to guarantee the required damping action for the displacement dynamics. In this case the setting drive must be designed in such a way that it can perform the tracking movement against that frictional damping action. The azimuthal or tower top mounting is usually in the form of a rolling bearing assembly.

Figure 7 is a partly sectional view of a known wind direction tracking system with an electrical setting drive from Westinghaus WTG-0600.

During operation of a wind power installation with turbulent winds – in dependence on the axis of rotation of the rotor – very high forces occur and, linked thereto, high and frequent load peaks in the azimuthal drives.

If there is more than one azimuthal drive, the situation additionally involves a very high degree of asymmetry in the individual drives. Those drives have a step-up transmission ratio by means of a transmission assembly of around 15,000. Very minor deviations in the tooth configuration at the periphery of the tower mounting result immediately in very severe asymmetries if more than one drive, for example four azimuthal drives, are mounted at the periphery of the tower mounting with an integrated tooth arrangement. Because of the high transmission step-up ratio those small deviations on the input side of the drive correspond to up to between 15 and 20 revolutions on the output side.

In consequence this means that, during and after each rotational procedure for the machine housing, the entire load and the entire rotary moment must be uniformly distributed if possible simultaneously to individual drives. In addition, when heavy azimuthal loads are involved, the drives should yield during the stoppage times when excessively high load levels occur, and permit easy rotary movement of the machine housing so that a suitable load relief effect can occur.

In addition, during the wind tracking movement of the machine housing of the wind power installation, in the event of severe turbulence, correspondingly high torques also occur. They excite the azimuthal drives

in such a way that the motors oscillate in mutually opposite relationship. In that case the transmission arrangements with their very high step-up transmission ratio react like a spring and the consequence is major torque fluctuations in the individual drives.

The object of the invention is to improve the azimuthal drive for wind power installations so that the above-indicated problems are eliminated, providing a structurally simple azimuthal drive, ensuring uniform load distribution for each azimuthal drive, and preventing unwanted torque fluctuations in the individual drives.

In accordance with the invention there is proposed a wind power installation as set forth in claim 1. Advantageous developments are described in the appendant claims.

The wind power installation according to the invention comprising a machine housing which accommodates a rotor with at least one rotor blades is distinguished in that the displacement device for displacement of the machine housing in accordance with the respective wind direction has as its azimuthal drive at least one three-phase asynchronous motor which is supplied with three-phase current during displacement of the machine housing and at times or completely with direct current during the stoppage time of the machine housing.

After the displacement operation by means of three-phase current the motors are switched off and thus no longer produce any torque. In order now also to provide for a braking action on the part of the drive motor and in order still to maintain an adequate braking torque during the stoppage time when load peaks occur, the three-phase asynchronous motor is acted upon by a direct current immediately after separation from the three-phase network. That direct current generates a stationary magnetic field in the asynchronous motor which is thereby immediately decelerated. As far as possible the direct current supply is maintained during the entire stoppage time.

In accordance with the invention there is provided a torque control for suppressing unwanted torque fluctuations. Deceleration of the three-phase asynchronous motor can be set linearly by means of the magnitude of the direct current. That affords a simple torque control for the azimuthal drives of wind power installations during the actual stoppage phase.

In addition, if the displacement device has a plurality of three-phase asynchronous motors, the three-phase asynchronous motors are coupled in negative feedback relationship by means of a current transformer so that the individual drive is stabilised and the hitherto unwanted spring effect is suppressed.

The invention is described in greater detail hereinafter by means of an embodiment with reference to the drawings in which:

Figure 1 diagrammatically shows an arrangement of four azimuthal drives of a displacement device on the machine housing,

Figure 2 shows a torque/rotary speed characteristic curve of a three-phase asynchronous motor,

Figures 3 shows the characteristic curve of a three-phase asynchronous motor in the direct-current mode of operation,

Figure 4 shows an alternative view in relation to Figure 3,

Figure 5 shows a block circuit diagram of a current transformer coupling of two asynchronous azimuthal drives,

Figure 6 shows a circuit diagram for an azimuthal motor, and

Figure 7 is a partly sectional view of a known wind tracking arrangement with an electric setting drive.

Wind power installations generally have an active drive for wind direction tracking. The active drive rotates the machine head of the wind power installation in such a way that the rotor blades of the rotor are oriented in optimum fashion in the direction of the wind.

The active drive for wind direction tracking is an azimuthal drive 1 with the associated azimuthal mounting 2 and is generally disposed

between the tower top and the machine housing. In the case of small wind power installations one azimuthal drive is sufficient, while larger wind power installations are usually provided with a plurality of drives, for example four drives as shown in Figure 1. The four drives are distributed uniformly around the periphery of the tower top 3 (a non-uniform distribution is also possible).

During operation of a wind power installation with turbulent winds – in dependence on the angle of rotation of the rotor – very high forces occur and, linked thereto, high and frequent load peaks in the azimuthal drives.

If the displacement device for displacement of the machine head has more than one azimuthal drive 1, a very high level of asymmetry additionally occurs in the individual drives 1. The drives have a step-up transmission arrangement 4 (transmission arrangement: not shown) with a step-up transmission ratio of about 15,000. Very small deviations in the tooth configuration of the transmission arrangements at the periphery of the tower mounting result immediately in very severe asymmetries if more than one drive is mounted at the periphery of the tower mounting with integrated tooth configuration. Because of the high transmission ratio those minor deviations on the input side of the drive correspond to up to between 15 and 20 revolutions on the output side.

That means that, during and after each rotary procedure of the tower top, the entire load/torque must be distributed uniformly to individual drives. In addition, in the event of heavy azimuthal loads, the drives should yield during the stoppage times – of the tower top – in the event of excessively high loads, and permit a slight rotary movement of the machine head.

Each azimuthal drive 1 has its own motor 5 and the motors are interconnected and are controlled jointly. If, during the wind tracking movement of the machine head of the wind power installation – caused by severe turbulence – major torques occur, those torques excite the

azimuthal drives in such a way that the motors oscillate in mutually opposite relationship or have a tendency to perform oscillations. The transmission arrangements 4 with their very high ratio react in that case like a spring, which results in major torque fluctuations in the individual drives.

In order to ensure uniform distribution of the loads during the time in which the machine housing is not rotated, it is proposed in accordance with the invention that, as drive motors for azimuthal drive purposes, a three-phase asynchronous motor is used as the asynchronous drive machine. The torque/rotary speed characteristic curve thereof is shown in Figure 2. M_A denotes the initial torque and M_K denotes the pull-out torque.

After the machine housing displacement operation the four three-phase asynchronous motors (ASM) are switched off and thus no longer produce any torque. In order to uniformly decelerate the motors and also thereafter still to obtain a braking torque, the motors are supplied with a direct current promptly after separation from the three-phase network, as far as possible immediately (see Figure 6a). That direct current produces a stationary magnetic field in the motors (asynchronous machine) which are thus immediately decelerated. That direct-current supply is maintained as far as possible during the entire stoppage time and can be regulated in respect of amplitude.

After the displacement operation the ASM-drives are supplied with a regulated direct current by means of a regulating device, as shown in Figure 6b. Slow rotary movements of the tower top which are caused by asymmetrical gusts of wind are only damped or attenuated by a low direct current (about 10% of the nominal current), but they are permitted. Faster rotary movements are prevented by a suitably adapted higher direct current and thus a higher braking moment. In the event of very fast rotary movements, the direct current is raised to the nominal current of the motor.

The torque/rotary speed characteristic curve of an asynchronous motor in the direct current mode of operation is shown in Figure 3. The drive motor does not generate any torque with the direct current magnetisation in the stopped condition. With increasing rotary speed however – up to about 6% of the nominal rotary speed – the torque generated rises linearly and this is symmetrical in both directions of rotation. In accordance with that characteristic curve, the load occurring is also distributed uniformly to all azimuthal drives and an equilibrium condition always passively occurs.

To provide for torque control in respect of the azimuthal drives, the gradient of the braking curve can be set linearly with the magnitude of the direct current. That is shown in Figure 4. That affords a simple torque control for the azimuthal drives of wind power installations during the actual stoppage phase.

It is further appropriate for the individual motors of the azimuthal drives to be couple by means of a current transformer. That is shown in Figure 5. In this case ASM denotes an asynchronous machine. Such a simple negative feedback as illustrated stabilises the drives.

Figure 7 shows a partly sectional view of a known wind direction tracking arrangement with an electrical setting drive, as is known from Erich Hau, "Windkraftanlagen" ("Wind Power Installations"), Springer-Verlag Berlin Heidelberg 1996, pages 268-271.

CLAIMS

1. A wind power installation comprising a machine housing which accommodates a rotor with at least one rotor blade and a displacement device for displacement of the machine housing for desired orientation of the rotor in the direction of the wind, wherein the displacement device has as its drive (1) a three-phase asynchronous motor which for displacement of the machine housing is acted upon by a three-phase current and is at times or completely acted upon with direct current during the stoppage time of the machine housing.

2. A wind power installation as set forth in claim 1 characterised in that the three-phase asynchronous motor is acted upon with the direct current after the three-phase current is switched off, for deceleration purposes.

3. A wind power installation as set forth in claim 1 or claim 2 characterised in that deceleration of the three-phase asynchronous motor at the end of the displacement operation is controlled by means of the magnitude of the direct current.

4. A wind power installation as set forth in one of the preceding claims characterised in that the displacement device has a plurality of three-phase asynchronous motors which are coupled together.

5. A wind power installation as set forth in claim 4 characterised in that the three-phase asynchronous motors are electrically coupled together by means of a current transformer.

Abstract

Wind power installations generally have an active drive for wind direction tracking. The active drive rotates the machine housing of the wind power installation in such a way that the rotor blades of the rotor are oriented in the direction of the wind. That drive which is required for wind direction tracking purposes is generally an azimuthal drive which is usually disposed with the associated azimuthal mountings between the tower top and the machine housing. One displacement drive is sufficient when small wind power installations are involved, while larger wind power installations are generally equipped with a plurality of azimuthal drives.

The object of the invention is to improve the azimuthal drive for wind power installations so that the above-indicated problems are eliminated, providing a structurally simple azimuthal drive, ensuring uniform load distribution for each azimuthal drive, and preventing unwanted torque fluctuations in the individual drives.

A wind power installation comprising a machine housing which accommodates a rotor with at least one rotor blade and a displacement device for displacement of the machine housing for desired orientation of the rotor in the direction of the wind, wherein the displacement device has as its drive a three-phase asynchronous motor which for displacement of the machine housing is acted upon by a three-phase current and is at times or completely acted upon with direct current during the stoppage time of the machine housing.

(Figure 3)

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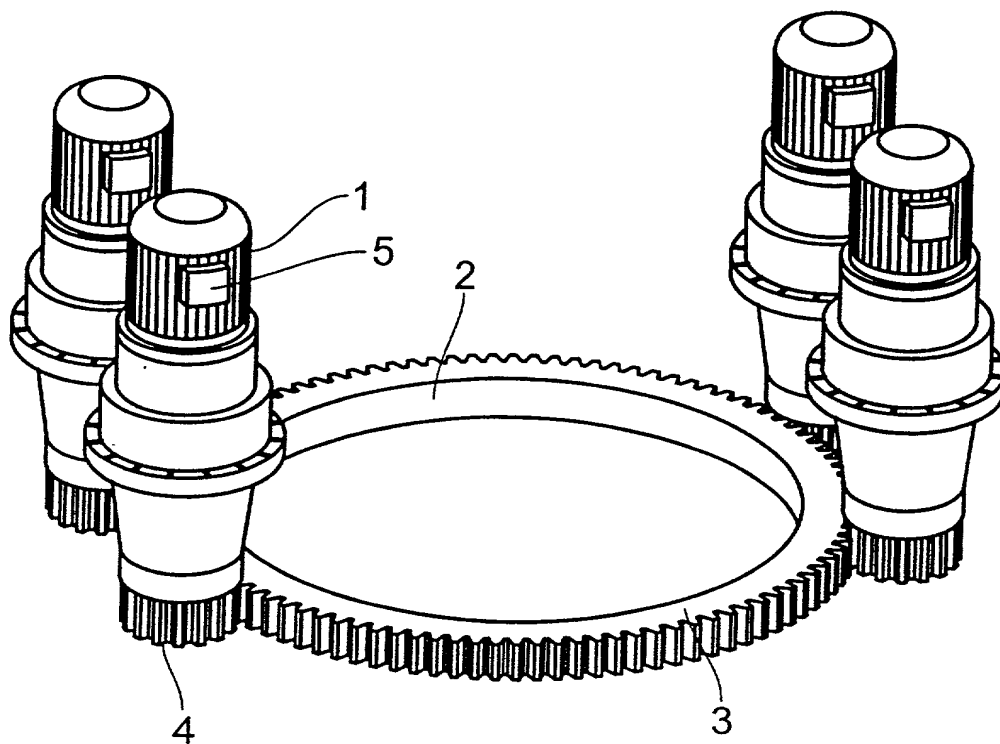


Fig. 1

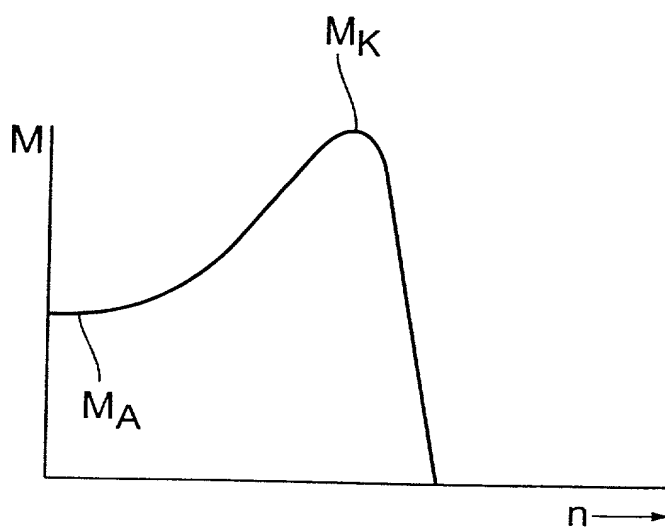


Fig. 2

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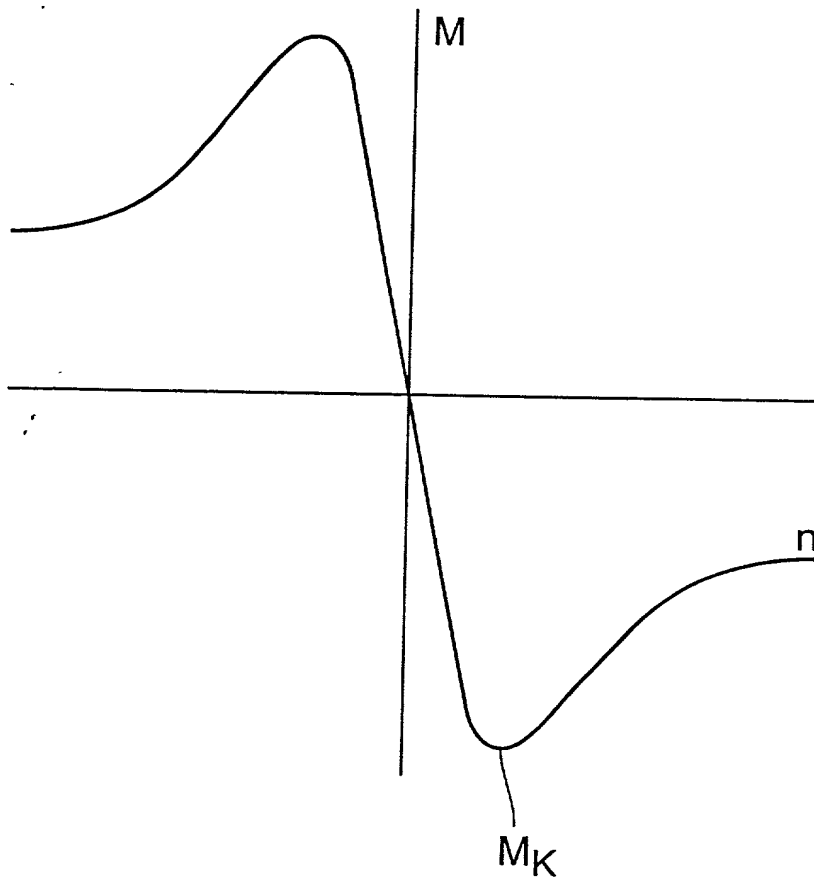


Fig. 3

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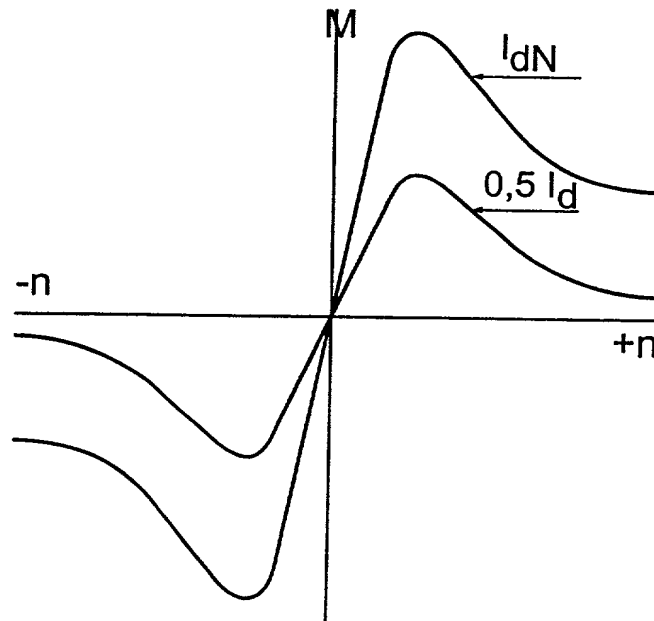


Fig. 4

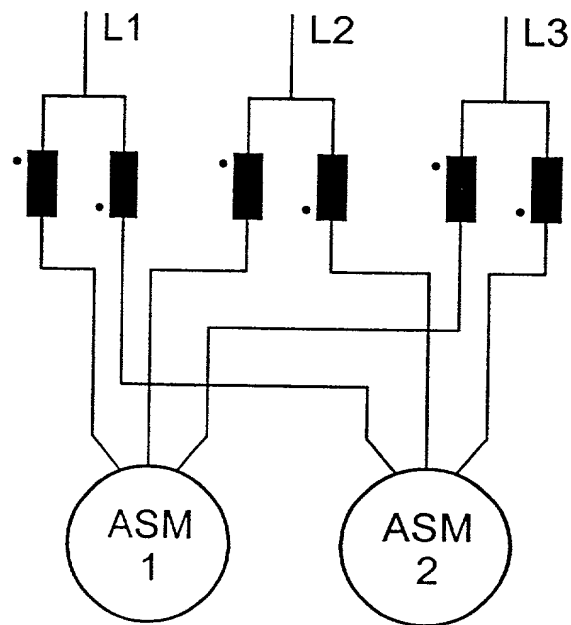


Fig. 5

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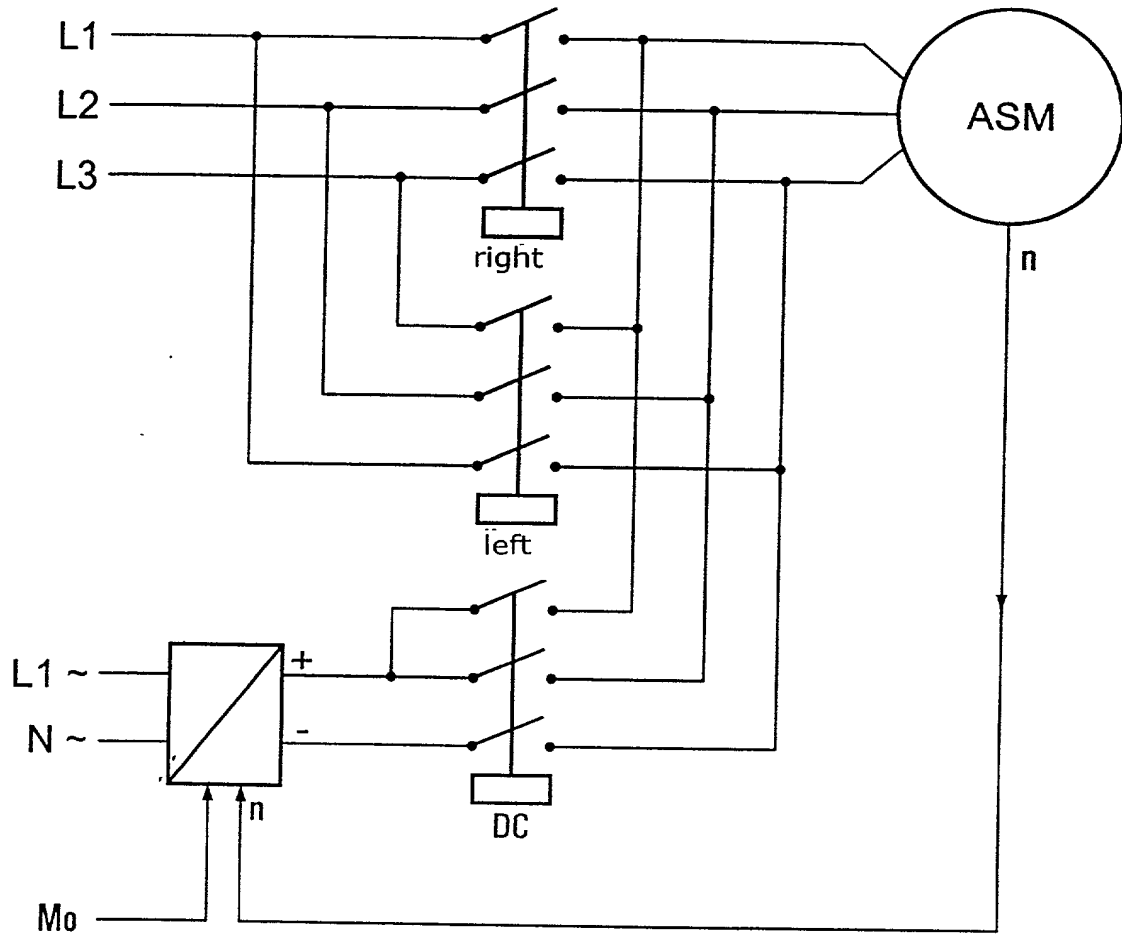


Fig. 6a

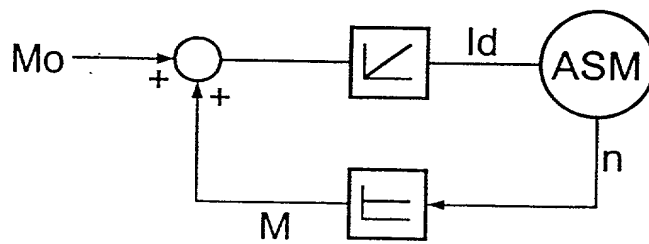


Fig. 6b

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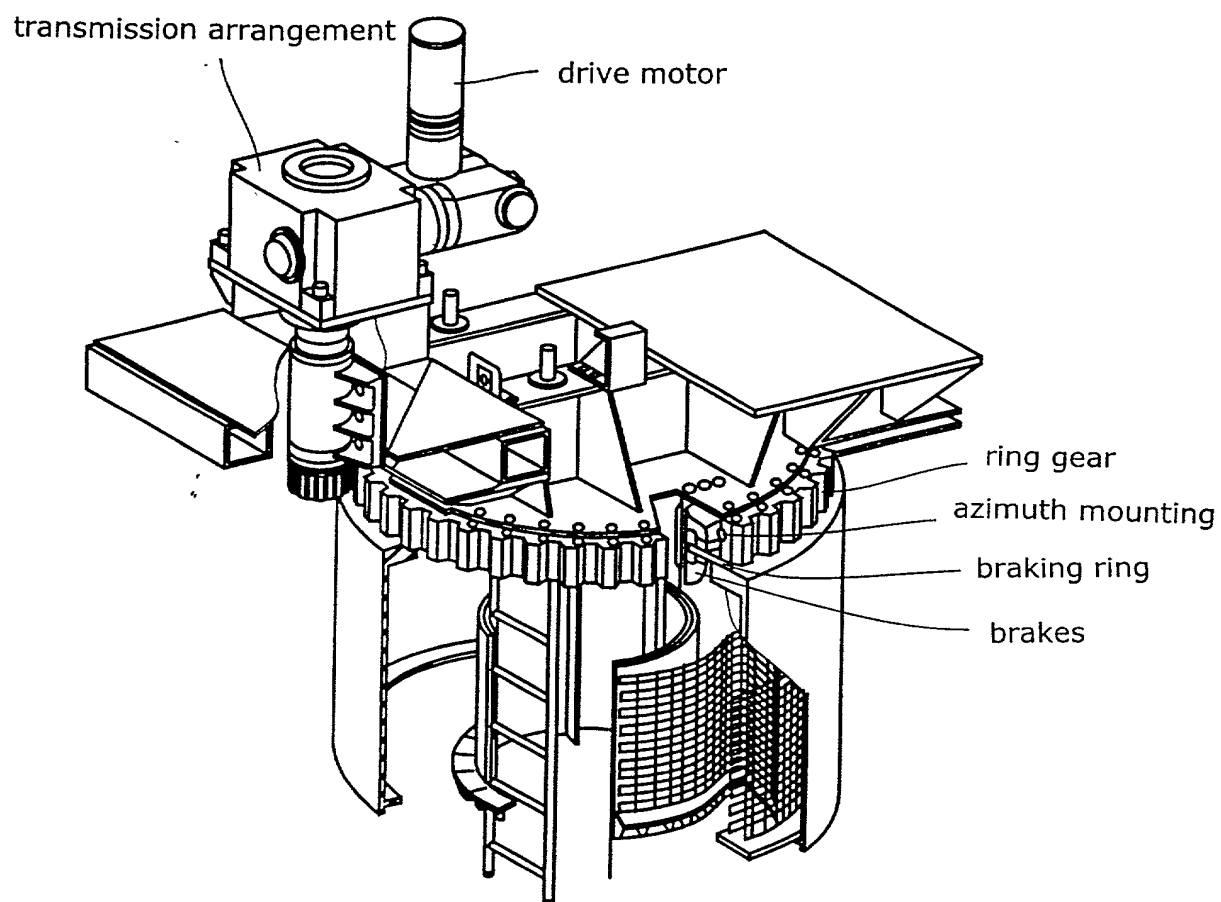


Fig. 7

DECLARATION AND POWER OF ATTORNEY

As the below-named inventor, I declare that:

My residence, post office address, and citizenship are as stated below under my name.

I believe I am the original, first, and sole inventor of the invention entitled "AZIMUTHAL DRIVING SYSTEM FOR WIND TURBINES," which is described and claimed in the specification and claims of International Patent Application No. PCT/EP99/07655, which was filed on 12 October 1999 and for which a patent is sought.

I have reviewed and understand the contents of the above-identified specification and claims, as amended by any amendment specifically referred to herein (if any). I acknowledge my duty to disclose information of which I am aware which is material to the patentability and examination of this application in accordance with 37 C.F.R. § 1.56(a).

I hereby claim foreign priority benefits under 35 U.S.C. § 119 of the foreign patent application listed below:

PRIOR FOREIGN/PCT APPLICATION(S) AND ANY PRIORITY CLAIMS UNDER 35 U.S.C. 119:			
COUNTRY	APPLICATION NUMBER	DATE OF FILING	PRIORITY CLAIMED UNDER 35 USC 119
Germany	19854683.1	26 November 1998	Yes
Germany	19920504.3	5 May 1999	Yes

27

I hereby appoint George C. Rondeau, Jr., Reg. No. 28,893; David H. Deits, Reg. No. 28,066; William O. Ferron, Jr., Reg. No. 30,633; Richard G. Sharkey, Reg. No. 32,629; David V. Carlson, Reg. No. 31,153; Karl R. Hermanns, Reg. No. 33,507; Michael J. Donohue, Reg. No. 35,859; Jane E. R. Potter, Reg. No. 33,332; Robert Iannucci, Reg. No. 33,514; Lorraine Linford, Reg. No. 35,939; David W. Parker, Reg. No. 37,414; E. Russell Tarleton, Reg. No. 31,800; Ellen M. Bierman, Reg. No. 38,079; Brian G. Bodine, Reg. No. 40,520; Robert M. Ward, Reg. No. 26,517; Frank Abramonte, Reg. No. 38,066; Kevin S. Costanza, Reg. No. 37,801; Thomas E. Loop, Reg. No. 42,810; Stephen J. Rosenman, Reg. No. 43,058; Brian L. Johnson, Reg. No. 40,033; Susan D. Betcher, Reg. No. 43,498; William T. Christiansen, Reg. No. 44,614; Eric J. Gash, Reg. No. 46,274; Jeffrey C. Pepe, Reg. No. 46,985; Charles J. Rupnick, Reg. No. 43,068; Timothy L. Boller, Reg. No. 47,435; and James M. Verna, Reg. No. 33,287; comprising the firm of Seed Intellectual Property Law Group PLLC,

701 Fifth Avenue, Suite 6300, Seattle, Washington 98104-7092, as my attorneys to prosecute this application and transact all business in the Patent and Trademark Office connected therewith. Please direct all telephone calls to **Eric J. Gash** at (206) 622-4900 and telecopies to (206) 682-6031.

I further declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

1-00
Aloys Wobben

Date 5.7.01

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